

A Contribution to the Microwave Spectrum of Dimethyl Selenide *

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The microwave spectra of five isotopic species of dimethyl selenide have been measured and analysed for centrifugal distortion and internal rotation by PAM and IAM.

We investigated the rotational spectra of five isotopic species of dimethyl selenide: $(\text{CH}_3)_2^{\text{n}}\text{Se}$, $n = 76, 77, 78, 80, 82$. The most abundant 78- and 80-isotopic species have been assigned and analysed earlier by Beecher [1]. Our aim was to determine the centrifugal distortion and the hindering potential of internal rotation for comparison between the isotopic species and for a precise prediction of the ground state rotational spectra. We hope hereby to assist the assignment of rotational spectra of torsional excited states currently under investigation for the determination of V'_{12} [2–4].

Further we compared the two fundamental methods for the analysis of internal rotation: PAM and IAM [5, 6] which was not yet done for many molecules.

Experimental

The spectra were measured by conventional Stark spectrometers [7, 8] with 33 and 100 kHz modulation frequency. The substance was supplied by Ventron GmbH, Karlsruhe, and used after vacuum distillation.

Analysis and Results

The spectra of the 76-, 77- and 82-isotopic species were assigned with the help of the Stark effect and the similarity of the torsional fine structure after a prediction of the spectra based on the structure [1].

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For the centrifugal distortion analysis the AA-components of the torsion fine structure of the transitions given in Table 1 were used. The analysis was performed with the help of the programs VT 26 and VT 27 written by Typke [9] based on the Hamiltonian of Watson [10].

$$H = A P_z^2 + B P_x^2 + C P_y^2 - \Delta_J P^4 - \Delta_{JK} P^2 P_z^2 - \Delta_K P_z^4 - \delta_J [P^2 (P_x^2 - P_y^2) + (P_x^2 - P_y^2) P^2] - \delta_K [P_z^2 (P_x^2 - P_y^2) + (P_x^2 - P_y^2) P_z^2]. \quad (1)$$

The least square fitted rotational constants, centrifugal distortion parameters and derived parameters together with standard errors are given in Table 2. The highest correlation coefficient is $|\Delta_{JK}, \delta_K| = 0.97$, as can be seen from Table 3.

The rotational constants show the usual change with the isotopic mass. This cannot be stated for the centrifugal distortion constants.

The torsion fine structure was analysed by using the multiplet splittings of Table 1.

The Hamiltonian

$$H = A P_z^2 + B P_x^2 + C P_y^2 + F (p_1 - p_1)^2 + F (p_2 - p_2)^2 + \frac{V_3}{2} (1 - \cos 3 \alpha_1) + \frac{V_3}{2} (1 - \cos 3 \alpha_2) + F' \{ (p_1 - p_1) (p_2 - p_2) + (p_2 - p_2) (p_1 - p_1) \} \quad (2)$$

without centrifugal distortion terms proved to be sufficient to calculate the torsional splittings. The meaning of the symbols of (2) are given for example in [3].

For the PAM-analysis the Hamiltonian was treated by fourth order van Vleck perturbation theory including denominator correction. A modified program originally written by Rudolph, Schleser and Tan was used. The results are given in Table 4 with V_3 and θ fitted.

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Table 1a–e. Measured transitions of dimethyl selenide for the 76, 77, 78, 80 and 82-Selenium isotopes. The measured frequencies ν_{exp} are given in the order of the symmetry species A_1A_1 , EE , A_1E , EA_1 . $\Delta\nu_{\text{exp}}$ gives the torsional splitting referred to the A_1A_1 component. $\nu_{\text{calc}}^{(A_1A_1)}$ was calculated with Hamiltonian (1). $\Delta\nu_{\text{calc}}^{(\text{PAM})}$ and $\Delta\nu_{\text{calc}}^{(\text{IAM})}$ are the calculated torsional splittings with the deviation $\delta\nu$. All frequencies in MHz.

Transition $J_{K-K_+} - J_{K'-K'_+}$	ν_{exp}	$\Delta\nu_{\text{exp}}$	$\nu_{\text{calc}}^{(A_1A_1)}$	$\Delta\nu_{\text{calc}}^{\text{PAM}}$	$\delta\nu$	$\Delta\nu_{\text{calc}}^{\text{IAM}}$	$\delta\nu$
(CH ₃) ₂ ⁷⁶ Se							
1 ₁₁ - 0 ₀₀	15994.500		15994.440	0.060			
	15993.830	0.620	0.645	-0.025	0.644	-0.024	
	15993.250	1.250	1.258	-0.008	1.257	-0.007	
	15993.250	1.250	1.322	-0.072	1.320	-0.070	
2 ₁₁ - 2 ₀₂	9962.800		9962.834	-0.034			
	9962.021	0.779	0.807	-0.028	0.810	-0.031	
	9961.219	1.581	1.617	-0.036	1.630	-0.049	
	9961.219	1.581	1.608	-0.027	1.608	-0.027	
2 ₂₁ - 2 ₁₂	20673.570		20673.579	-0.009			
	20671.461	2.109	2.088	0.021	2.073	0.036	
	20669.796	3.774	3.763	0.011	3.752	0.022	
	20669.147	4.423	4.588	-0.165	4.540	-0.117	
2 ₁₂ - 1 ₀₁	25097.603		25097.548	0.055			
	25097.023	0.580	0.629	-0.049	0.631	-0.051	
	25096.400	1.203	1.246	-0.043	1.252	-0.049	
	25096.400	1.203	1.271	-0.068	1.273	-0.070	
2 ₂₁ - 1 ₁₀	38879.717		38879.693	0.024			
	38877.685	2.032	2.105	-0.073	2.092	-0.060	
	38876.024	3.693	3.758	-0.065	3.747	-0.054	
	A		4.662		4.620		
3 ₂₁ - 3 ₁₂	13792.978		13792.973	0.005			
	13791.700	1.278	1.274	0.004	1.270	0.003	
	13790.374	2.604	2.622	-0.018	2.621	-0.017	
	13790.494	2.484	2.474	0.010	2.470	0.014	
3 ₁₂ - 3 ₀₃	15469.834		15469.861	-0.027			
	15468.669	1.165	1.143	0.022	1.150	0.015	
	15467.516	2.318	2.290	0.028	2.300	0.018	
	15467.516	2.318	2.280	0.038	2.289	0.029	
3 ₂₂ - 3 ₁₃	24608.954		24608.945	0.011			
	24606.739	2.215	2.166	0.049	2.161	0.054	
	24604.460	4.494	4.250	0.244	4.242	0.252	
	24604.460	4.494	4.413	0.081	4.394	0.100	
3 ₁₃ - 2 ₀₂	33336.896		33336.995	-0.099			
	33336.390	0.506	0.554	-0.048	0.556	-0.050	
	33335.856	1.040	1.099	-0.059	1.111	-0.071	
	33335.856	1.040	1.116	-0.076	1.122	-0.082	
4 ₂₂ - 4 ₁₃	15345.927		15345.937	-0.010			
	15344.661	1.266	1.274	-0.008	1.278	-0.012	
	15343.384	2.543	2.564	-0.021	2.584	-0.041	
	15343.384	2.543	2.534	0.009	2.535	0.008	
4 ₁₃ - 4 ₀₄	23284.510		23284.513	-0.003			
	23282.820	1.690	1.663	0.027	1.671	0.019	
	23281.160	3.350	3.336	0.014	3.342	0.008	
	23281.160	3.350	3.317	0.033	3.334	0.016	
4 ₃₂ - 4 ₂₃	30605.310		30605.296	0.014			
	30602.235	3.075	3.128	-0.053	3.076	-0.001	
	30599.792	5.518	5.552	-0.034	5.535	-0.017	
	30598.591	6.719	6.959	-0.240	6.768	-0.049	
4 ₃₁ - 4 ₂₂	23371.560		23371.547	0.013			
	23369.500	2.060	2.035	0.025	2.057	0.003	
	23366.830	4.730	4.773	-0.043	4.734	-0.004	
	23368.060	3.500	3.369	0.131	3.502	-0.002	
4 ₂₃ - 4 ₁₄	29861.862		29861.861	0.001			
	29859.405	2.457	2.473	-0.016	2.471	-0.014	
	29856.944	4.918	4.919	-0.001	4.914	0.004	
	29856.944	4.918	4.972	-0.054	4.964	-0.046	
5 ₃₂ - 5 ₂₃	21270.180		21270.173	0.007			
	21268.170	2.010	2.013	-0.003	2.016	-0.006	
	21266.010	4.170	4.197	-0.027	4.180	-0.010	
	21266.280	3.900	3.856	0.044	3.883	0.017	
5 ₂₃ - 5 ₁₄	19661.760		19661.774	-0.014			
	19660.350	1.410	1.416	-0.006	1.424	-0.014	
	19658.920	2.840	2.838	0.002	2.863	-0.023	
	19658.920	2.840	2.826	0.014	2.844	-0.004	
6 ₃₃ - 6 ₂₄	21080.450		21080.461	-0.011			
	21078.640	1.810	1.819	-0.009	1.828	-0.018	
	21076.840	3.610	3.683	-0.073	3.703	-0.093	
	21076.840	3.610	3.594	0.016	3.605	0.005	
6 ₂₄ - 6 ₁₅	26852.739		26852.726	0.013			
	26850.941	1.798	1.774	0.024	1.785	0.013	
	26849.162	3.577	3.559	0.018	3.578	-0.001	
	26849.162	3.577	3.537	0.040	3.568	0.009	
6 ₄₂ - 6 ₃₃	32994.562		32994.577	-0.015			
	32991.755	2.807	2.702	0.105	2.816	-0.009	
	32987.851	6.711	6.695	0.016	6.633	0.078	
	32989.887	4.675	4.122 ^c	0.553	4.645	0.030	
6 ₃₃ - 5 ₄₂	38918.526		38918.501	0.025			
	B		-5.656		-5.015		
	B		-4.871		-4.757		
	B		-17.210		-14.945		
7 ₄₃ - 7 ₃₄	29570.939		29570.941	-0.002			
	29568.126	2.813	2.776	0.037	2.809	0.004	
	29565.054	5.885	5.912	-0.027	5.875	0.010	
	29565.570	5.369	5.195	0.174	5.348	0.021	
7 ₃₄ - 7 ₂₅	23836.570		23836.568	0.002			
	23834.820	1.750	1.731	0.019	1.738	0.012	
	23833.090	3.460	3.473	0.007	3.508	-0.028	
	23833.090	3.480	3.451	0.029	3.473	0.007	
7 ₄₃ - 6 ₅₂	36445.481		36445.491	-0.010			
	B		-22.952		-18.968		
	B		-6.994		-6.875		
	B		-57.481		-48.535		
8 ₄₄ - 8 ₃₅	27574.627		27574.619	0.008			
	27572.169	2.458	2.442	0.016	2.457	0.001	
	27569.740	4.887	4.994	-0.107	5.000	-0.113	
	27569.740	4.887	4.775	0.112	4.828	0.059	
8 ₃₅ - 8 ₂₆	29926.037		29926.054	-0.017			
	29924.163	1.874	1.870	0.004	1.887	-0.013	
	29922.252	3.785	3.750	0.035	3.789	-0.004	
	29922.252	3.785	3.728	0.057	3.773	0.012	
9 ₄₅ - 9 ₃₆	28463.000		28462.990	0.010			
	28460.864	2.136	2.122	0.014	2.148	-0.012	
	28458.649	4.351	4.274	0.077	4.328	0.023	
	28458.649	4.351	4.215	0.136	4.266	0.085	

Table 1b.

Transition $J_{K-K_+} - J'_{K'-K'_+}$	r_{exp}	Δr_{exp}	$r_{\text{calc}}^{(\text{A1A1})} \Delta r_{\text{PAM}}^{\text{calc}}$	δr	$\Delta r_{\text{calc}}^{\text{IAM}}$	δr
(CH₃)₂⁷⁷Se						
$2_{11} - 2_{02}$	9945.055 9944.254 9943.464 9943.464	 0.801 1.591 1.591	9945.047 0.799 1.602 1.593	0.008 0.002 -0.011 -0.002	0.802 0.802 1.614 1.593	-0.001 -0.023 -0.002
$2_{21} - 2_{12}$	20580.083 20578.074 20576.389 20575.639	 2.009 3.694 4.444	20580.103 2.060 3.718 4.521	-0.020 -0.051 -0.024 -0.077	2.046 2.046 3.709 4.477	-0.037 -0.015 -0.033
$2_{12} - 1_{01}$	25042.952 25042.336 25041.722 25041.722	 0.615 1.230 1.230	25042.906 0.621 1.231 1.255	0.046 -0.005 -0.001 -0.025	0.625 0.625 1.238 1.259	-0.009 -0.008 -0.029
$2_{21} - 1_{10}$	38762.762 38760.695 38759.035 38758.283	 2.067 3.727 4.479	38762.735 2.077 3.714 4.593	0.027 -0.010 0.013 -0.114	2.065 2.065 3.705 4.555	0.002 0.022 -0.076
$3_{21} - 3_{12}$	13708.925 13707.667 13706.344 13706.467	 1.258 2.581 2.458	13708.925 1.256 2.584 2.441	0.000 0.002 -0.003 0.017	1.254 1.254 2.586 2.458	0.004 0.005 0.020
$3_{12} - 3_{03}$	15476.204 15475.059 15473.927 15473.927	 1.145 2.277 2.277	15476.200 1.135 2.276 2.265	0.004 0.010 0.001 0.012	1.143 1.143 2.285 2.274	0.002 -0.008 0.003
$3_{22} - 3_{13}$	24528.103 24526.029 24523.875 24523.875	 2.074 4.228 4.228	24528.151 2.142 4.205 4.364	-0.048 -0.068 0.023 -0.136	2.139 2.139 4.199 4.346	-0.065 0.029 -0.113
$3_{13} - 2_{02}$	33271.191 33270.612 33270.052 33270.052	 0.579 1.139 1.139	33271.205 0.546 1.085 1.101	-0.014 0.033 0.054 0.038	0.549 0.549 1.099 1.109	0.030 0.040 0.030
$3_{12} - 2_{21}$	23905.440 23906.350 23906.800 23907.640	 -0.910 -1.360 -2.200	23905.480 -0.907 -1.394 -2.232	-0.040 -0.003 0.034 +0.032	-0.880 -0.880 -1.365 -2.164	-0.030 0.005 -0.036
$4_{22} - 4_{13}$	15299.778 15298.513 15297.250 15297.250	 1.265 2.528 2.528	15299.785 1.260 2.534 2.505	-0.007 0.005 -0.006 0.023	1.262 1.262 2.555 2.506	0.003 -0.027 0.022
$4_{13} - 4_{04}$	23311.480 23309.820 23308.140 23308.140	 1.660 3.340 3.340	23311.451 1.656 3.321 3.302	0.029 0.004 0.019 0.038	1.662 1.662 3.324 3.316	-0.002 0.016 0.024
$4_{32} - 4_{23}$	30454.242 30451.195 30448.749 30447.563	 3.047 5.493 6.679	30454.229 3.081 5.483 6.840	0.013 -0.034 0.010 -0.161	3.031 3.031 5.465 6.654	0.016 0.028 0.025
$4_{31} - 4_{22}$	23176.250 23174.170 23171.590 23172.760	 2.080 4.660 3.490	23176.257 2.010 4.699 3.345	-0.007 0.070 -0.039 0.145	2.035 2.035 4.664 3.475	0.045 -0.004 0.015
$4_{23} - 4_{14}$	29796.132 29793.692 29791.206 29791.206	 2.440 4.926 4.926	29796.158 2.449 4.872 4.923	-0.026 -0.009 0.054 0.003	2.449 2.449 4.871 4.919	-0.009 0.055 0.007
$5_{32} - 5_{23}$	21102.390 21100.400 21098.290 21098.570	 1.990 4.100 3.820	21102.408 1.982 4.128 3.800	-0.018 0.008 -0.028 0.020	1.984 1.984 4.117 3.832	0.006 -0.017 -0.012
$5_{23} - 5_{14}$	19669.560 19668.150 19666.740 19666.740	 1.410 2.820 2.820	19669.555 1.405 2.816 2.804	0.005 0.005 0.004 0.016	1.412 1.412 2.836 2.814	-0.002 -0.015 0.006
$6_{33} - 6_{24}$	30974.740 30972.920 30971.150 30971.150	 1.820 3.590 3.590	30974.727 1.792 3.625 3.540	0.013 0.028 -0.035 0.050	1.801 1.801 3.648 3.555	0.019 -0.058 0.035
$6_{24} - 6_{15}$	26913.960 26912.178 26910.395 26910.395	 1.782 3.565 3.565	26913.927 1.767 3.546 3.524	0.033 0.015 0.019 0.041	1.777 1.777 3.563 3.553	0.005 0.002 0.012
$6_{42} - 6_{33}$	32692.293 32689.470 32685.698 32687.652	 2.823 6.595 4.641	32692.277 2.677 6.589 4.128 ^c	0.016 0.146 0.006 0.513	2.793 2.793 6.539 4.637	0.030 0.056 0.004
$7_{43} - 7_{34}$	29290.152 29287.389 29284.373 29284.862	 2.763 5.779 5.290	29290.161 2.731 5.805 5.120	-0.009 0.032 -0.026 0.170	2.766 2.766 5.781 5.277	-0.003 -0.002 0.013
$7_{34} - 7_{25}$	23819.390 23817.660 23815.950 23815.950	 1.730 3.440 3.440	23819.381 1.711 3.432 3.411	0.009 0.019 0.008 0.029	1.719 1.719 3.469 3.434	0.011 -0.029 0.006
$7_{43} - 6_{52}$	36814.844 B B B	 	36814.841 -22.294 -6.867 -56.286	0.003 	-18.418 -6.757 -47.519	
$8_{44} - 8_{35}$	27370.871 27368.461 27366.085 27366.035	 2.410 4.786 4.786	27370.880 2.398 4.899 4.692	-0.009 0.012 -0.113 0.094	2.410 2.410 4.906 4.746	0.000 -0.120 0.040
$8_{35} - 8_{26}$	30005.252 30003.356 30001.475 30001.475	 1.896 3.777 3.777	30005.281 1.859 3.729 3.706	-0.029 0.037 0.048 0.071	1.875 1.875 3.766 3.746	0.021 0.011 0.031
$9_{45} - 9_{36}$	28382.103 28379.975 28377.872 28377.872	 2.127 4.231 4.231	28382.090 2.088 4.203 4.148	0.013 0.039 0.028 0.083	2.117 2.117 4.266 4.211	0.010 -0.035 0.020

Table 1 c.

Transition $J_{K-K_+} - J_{K-K_+}'$	ν_{exp}	$\Delta\nu_{\text{exp}}$	$\nu_{\text{calc}}^{(\text{A}_1\text{A}_1)} \Delta\nu_{\text{calc}}^{\text{PAM}}$	$\delta\nu$	$\Delta\nu_{\text{calc}}^{\text{IAM}}$	$\delta\nu$
(CH₃)₂⁷⁸Se						
1 ₁₁ - 0 ₀₀	15909.836 15909.224 15908.604 15908.604	 0.612 1.232 1.232	15909.879 0.632 1.234 1.296	-0.043 -0.020 -0.002 -0.064	0.633 1.235 1.297	-0.021 -0.003 -0.065
2 ₁₁ - 2 ₀₂	9927.907 9927.119 9926.332 9926.332	 0.788 1.575 1.575	9927.905 0.796 1.595 1.587	0.002 -0.008 -0.020 -0.012	0.799 1.608 1.587	-0.011 -0.033 -0.012
2 ₂₁ - 2 ₁₂	20489.318 20487.285 20485.618 20484.677	 2.033 3.700 4.441	20489.306 2.044 3.693 4.482	0.012 -0.011 0.007 -0.041	2.033 3.688 4.442	0.000 0.012 -0.001
2 ₁₂ - 1 ₀₁	24989.687 24989.073 A A	 0.614 1.222 1.247	24989.730 0.617 1.222 1.251	-0.043 -0.003 0.621 1.251	-0.007 1.230 1.251	 -0.007 -0.007
2 ₂₁ - 1 ₁₀	38649.012 38646.975 38645.350 38644.527	 2.037 3.662 4.485	38649.027 2.060 3.688 4.553	-0.015 -0.023 -0.026 -0.068	2.051 3.684 4.521	-0.014 -0.022 -0.036
3 ₂₁ - 3 ₁₂	13627.585 13626.341 13625.042 13625.161	 1.244 2.543 2.424	13627.588 1.244 2.559 2.419	-0.003 0.000 -0.016 0.005	1.244 2.566 2.421	0.000 -0.023 0.003
3 ₁₂ - 3 ₀₃	15482.654 15481.525 15480.385 15480.385	 1.129 2.269 2.269	15482.647 1.135 2.275 2.264	0.007 -0.006 -0.006 0.005	1.139 2.278 2.268	-0.010 -0.009 0.001
3 ₂₂ - 3 ₁₃	24449.824 24447.659 24445.540 24445.540	 2.165 4.284 4.284	24449.790 2.130 4.182 4.339	0.034 0.035 0.102 -0.055	2.128 4.180 4.324	0.037 0.104 -0.040
3 ₁₂ - 2 ₂₁	23998.430 23999.310 23999.820 24000.580	 -0.880 -1.390 -2.150	23998.337 -0.887 -1.361 -2.185	0.093 +0.007 -0.029 0.035	-0.866 -1.345 -2.130	-0.014 -0.045 -0.020
4 ₂₂ - 4 ₁₃	15255.680 15254.426 15253.178 15253.178	 1.254 2.502 2.502	15255.670 1.251 2.516 2.488	0.010 0.003 -0.014 0.014	1.255 2.537 2.490	-0.001 -0.035 0.012
4 ₁₃ - 4 ₀₄	23337.790 23336.110 23334.450 23334.450	 1.680 3.340 3.340	23337.792 1.658 3.325 3.307	-0.002 0.022 0.015 0.033	1.660 3.320 3.313	0.020 0.020 0.027
4 ₃₂ - 4 ₂₃	30307.699 30304.681 30302.263 30301.104	 3.018 5.436 6.595	30307.664 3.052 5.442 6.765	0.035 -0.034 -0.006 -0.170	3.008 5.434 6.594	0.010 0.002 0.001
4 ₃₁ - 4 ₂₂	22986.640 22984.600 22982.000 22983.160	 2.040 4.640 3.480	22986.629 1.993 4.648 3.328	0.011 0.047 -0.008 0.152	2.023 4.629 3.469	0.017 0.011 0.011
4 ₂₃ - 4 ₁₄	29732.490 29730.032 29727.606 29727.606	 2.458 4.884 4.884	29732.573 2.438 4.851 4.902	-0.083 0.020 0.033 -0.018	2.438 4.852 4.899	0.020 0.032 -0.015
5 ₃₂ - 5 ₂₃	20940.320 20938.350 20936.250 20936.490	 1.970 4.070 3.830	20940.315 1.959 4.078 3.759	0.005 0.011 -0.008 0.071	1.967 4.078 3.799	0.003 -0.008 0.031
5 ₂₃ - 5 ₁₄	19678.250 19676.830 19675.430 19675.430	 1.420 2.820 2.820	19678.234 1.402 2.810 2.798	0.016 0.018 0.010 0.022	1.406 2.824 2.805	0.014 -0.004 0.015
6 ₃₃ - 6 ₂₄	20873.840 20872.060 20870.300 20870.300	 1.780 2.540 3.540	20873.839 1.772 3.586 3.504	0.001 0.008 -0.046 0.036	1.781 3.609 3.520	-0.001 -0.069 0.020
6 ₂₄ - 6 ₁₅	26974.438 26972.669 26970.854 26970.854	 1.769 3.584 3.584	26974.350 1.772 3.555 3.533	0.088 -0.003 0.029 0.051	1.773 3.555 3.541	-0.004 0.029 0.043
6 ₄₂ - 6 ₃₃	32398.466 32395.688 32391.974 32393.822	 2.778 6.492 4.644	32398.460 2.660 6.514 4.134 ^c	0.006 0.118 -0.022 0.510	2.785 6.492 4.652	-0.007 0.000 -0.008
7 ₄₃ - 7 ₃₄	29018.801 29016.038 29013.084 A	 2.763 5.717 5.065	29018.776 2.698 5.726 5.065	0.025 0.065 -0.009 0.025	2.738 5.719 5.226	0.025 -0.002 0.025
7 ₃₄ - 7 ₂₅	23805.350 23803.640 23801.930 23801.930	 1.710 3.420 3.420	23805.346 1.701 3.411 3.391	0.004 0.009 0.009 0.029	1.711 3.445 3.410	-0.001 -0.025 0.010
7 ₄₃ - 6 ₅₂	37173.062 B B B	 -21.810 -6.768 -55.466	37173.115 -21.810 -6.768 -55.466	-0.053 -18.035 -6.695 -46.851	 -18.035 -6.695 -46.851	 -18.035 -6.695 -46.851
8 ₄₄ - 8 ₃₅	27176.242 27173.859 27171.516 27171.516	 2.383 4.726 4.726	27176.277 2.364 4.829 4.630	-0.035 0.019 -0.103 0.096	2.391 4.859 4.699	-0.008 -0.133 0.027
8 ₃₅ - 8 ₂₆	30084.873 30083.017 30081.146 30081.146	 1.856 3.727 3.727	30084.960 1.862 3.734 3.711	-0.087 -0.006 -0.007 0.016	1.867 3.750 3.734	-0.011 -0.023 -0.007
8 ₅₃ - 7 ₆₂	36168.739 B B B	 -42.154 -8.505 -89.625	36168.707 -42.154 -8.505 -89.625	0.032 -34.492 -8.437 -73.492	 -34.492 -8.437 -73.492	 -34.492 -8.437 -73.492
9 ₄₅ - 9 ₃₆	28308.445 28306.342 28304.246 28304.246	 2.103 4.199 4.199	28308.445 2.065 4.156 4.103	0.000 0.038 0.043 0.096	2.086 4.203 4.141	0.017 -0.004 0.058
13 ₅₈ - 13 ₄₉	43467.452 43465.234 43462.984 43462.984	 2.218 4.468 4.468	43467.439 2.183 ^c 4.387 ^c 4.343 ^c	0.013 0.035 0.081 0.125	2.218 ^c 4.468 ^c 4.468 ^c	0.000 0.000 0.000

Table. 1 d. (Headline as on p. 1226).

(CH ₃) ₂ ⁸⁰ Se													
1 ₁₁ - 0 ₀₀	15829.140		15829.137	0.003			4 ₂₃ - 4 ₁₄	29610.131		29610.144	-0.013		
	15828.524	0.616	0.625	-0.009	0.624	-0.008		29607.710	2.421	2.417	0.004	2.409	0.012
	15827.900	1.240	1.220	0.020	1.217	0.023		29605.325	4.806	4.810	-0.004	4.795	0.011
	15827.900	1.240	1.282	-0.042	1.278	-0.038		29605.325	4.806	4.859	-0.053	4.841	-0.035
2 ₁₁ - 2 ₀₂	9895.202		9895.203	-0.001			5 ₃₂ - 5 ₂₃	20630.010		20630.001	0.009		
	9894.426	0.776	0.789	-0.013	0.790	-0.014		20628.080	1.930	1.928	0.002	1.930	0.000
	9893.643	1.559	1.582	-0.023	1.590	-0.031		20626.040	3.970	4.007	-0.037	3.992	-0.022
	9893.643	1.559	1.573	-0.014	1.570	-0.011		20626.260	3.750	3.705	0.045	3.727	0.023
2 ₂₁ - 2 ₁₂	20314.170		20314.119	0.051			5 ₂₃ - 5 ₁₄	19698.060		19698.054	0.006		
	20312.152	2.018	2.015	0.002	2.000	0.018		19696.660	1.400	1.390	0.010	1.391	0.009
	20310.472	3.698	3.651	0.047	3.636	0.062		19695.270	2.790	2.785	0.005	2.797	-0.007
	20309.818	4.352	4.415	-0.063	4.363	-0.011		19695.270	2.790	2.773	0.017	2.777	0.013
2 ₂₀ - 2 ₁₁	13901.585		13901.577	0.008			6 ₃₃ - 6 ₂₄	20684.320		20684.313	0.007		
	13900.396	1.189	1.190	-0.001	1.188	0.001		20682.580	1.740	1.741	-0.001	1.746	-0.006
	13898.844	2.741	2.761	-0.020	2.740	0.001		20680.850	3.470	3.521	-0.051	3.539	-0.069
	13899.563	2.022	2.000	0.022	2.013	0.009		20680.850	3.470	3.446	0.024	3.453	0.017
2 ₁₂ - 1 ₀₁	24886.683		24886.689	-0.006			6 ₂₄ - 6 ₁₅	27093.345		27093.245	0.100		
	24886.109	0.574	0.610	-0.036	0.611	-0.037		27091.573	1.772	1.766	0.006	1.766	0.006
	24885.574	1.109	1.208	-0.099	1.213	-0.104		27089.763	3.582	3.543	0.039	3.539	0.043
	24885.574	1.109	1.233	-0.124	1.233	-0.124		27089.763	3.582	3.520	0.062	3.525	0.057
2 ₂₁ - 1 ₁₀	38429.208		38429.200	0.008			6 ₄₂ - 6 ₃₃	31831.062		31831.069	-0.007		
	38427.199	2.009	2.034	-0.025	2.018	-0.009		31823.315	2.747	2.649	0.098	2.746	0.001
	38425.597	3.611	3.648	0.037	3.631	-0.020		31824.664	6.398	6.414	-0.016	6.352	0.046
	38424.784	4.424	4.487	-0.063	4.439	-0.015		31826.424	4.638	4.185 ^c	0.453	4.637	0.001
3 ₂₁ - 3 ₁₂	13471.513		13471.502	0.011			7 ₄₃ - 7 ₃₄	28498.981		28498.962	0.019		
	13470.285	1.228	1.227	0.001	1.224	0.004		28496.297	2.684	2.654	0.030	2.676	0.008
	13469.000	2.513	2.522	-0.009	2.521	-0.008		28493.392	5.589	5.618	-0.029	5.586	0.003
	13469.115	2.398	2.387	0.011	2.382	0.016		28493.835	5.146	5.000	0.146	5.133	0.013
3 ₁₂ - 3 ₀₃	15495.838		15495.832	0.006			7 ₃₄ - 7 ₂₅	23785.700		23785.701	-0.001		
	15494.713	1.125	1.128	-0.003	1.131	-0.006		23784.010	1.690	1.676	0.014	1.680	0.010
	15493.580	2.258	2.261	-0.003	2.262	-0.004		23782.330	3.370	3.362	0.008	3.383	-0.013
	15493.580	2.258	2.251	0.007	2.251	0.007		23782.330	3.370	3.343	0.027	3.348	0.022
3 ₂₂ - 3 ₁₃	24298.808		24298.800	0.008			7 ₄₃ - 6 ₅₂	37879.134		37879.125	0.009		
	24296.705	2.103	2.108	-0.005	2.101	0.002		B		-20.911		-17.191	
	24294.555	4.253	4.140	0.113	4.127	0.126		B		-6.658		-6.539	
	24294.555	4.253	4.292	-0.039	4.267	-0.014		B		-53.929		-45.328	
3 ₁₃ - 2 ₀₂	33083.282		33083.298	-0.016			8 ₄₄ - 8 ₃₅	26810.126		26810.127	-0.001		
	33082.796	0.486	0.535	-0.049	0.537	-0.051		26807.798	2.328	2.315	0.013	2.328	0.000
	33082.297	0.985	1.063	-0.078	1.073	-0.088		26805.481	4.645	4.723	-0.078	4.734	-0.089
	33082.297	0.985	1.079	-0.094	1.083	-0.098		26805.481	4.645	4.539	0.106	4.590	0.055
3 ₁₂ - 2 ₂₁	24177.670		24177.667	0.003			8 ₃₅ - 8 ₂₆	30245.790		30245.901	-0.111		
	24178.510	-0.840	-0.861	0.021	-0.836	-0.004		30243.923	1.867	1.848	0.019	1.852	0.015
	24178.980	-1.310	-1.323	0.013	-1.298	-0.062		30242.070	3.720	3.708	0.012	3.719	0.001
	24179.740	-2.070	-2.122	0.052	-2.056	-0.014		30242.070	3.720	3.684	0.036	3.703	0.017
4 ₂₂ - 4 ₁₃	15172.574		15172.567	0.007			8 ₅₃ - 7 ₆₂	36951.217		36951.215	0.002		
	15171.342	1.232	1.235	-0.003	1.234	-0.002		B		-41.465		-33.835	
	15170.111	2.463	2.483	-0.020	2.496	-0.033		B		-8.376		-8.253	
	15170.111	2.463	2.456	0.007	2.451	0.012		B		-88.325		-72.304	
4 ₁₃ - 4 ₀₄	23388.760		23388.764	-0.004			9 ₄₅ - 9 ₃₆	28180.278		28180.268	0.010		
	23387.110	1.650	1.652	-0.002	1.653	-0.003		28178.228	2.050	2.022	0.028	2.047	0.003
	23385.470	3.290	3.313	-0.023	3.307	-0.017		28176.184	4.094	4.068	0.026	4.109	-0.015
	23385.470	3.290	3.295	-0.005	3.299	-0.009		28176.184	4.094	4.021	0.073	4.055	0.039
4 ₃₂ - 4 ₂₃	30025.309		30025.383	-0.074			9 ₆₃ - 8 ₇₂	37065.492		37065.498	-0.006		
	30022.369	2.940	3.003	-0.063	2.953	-0.013		B		-58.978		-44.984	
	30019.972	5.337	5.377	-0.040	5.352	-0.015		B		-9.989		-9.859	
	30018.884	6.425	6.636 ^c	-0.211	6.449	-0.024		B		-130.234		-97.835	
4 ₃₁ - 4 ₂₂	22620.950		22620.946	0.004			13 ₅₈ -13 ₄₉	43871.521		43871.508	0.013		
	22618.960	1.990	1.974	0.016	1.994	-0.004		43869.306	2.215	2.165 ^c	0.050	2.203 ^c	0.012
	22616.410	4.540	4.578	-0.038	4.539	0.001		43867.088	4.433	4.353 ^c	0.080	4.437 ^c	-0.004
	22617.500	3.450	3.321	0.129	3.439	0.011		43867.088	4.433	4.307 ^c	0.126	4.437 ^c	-0.004

Table 1e.

Transition $J_{K-K_+} - J'_{K'-K'_+}$	ν_{exp}	$\Delta \nu_{\text{exp}}$	$\nu_{\text{calc}}^{(\text{A}_1, \text{A}_1)} \Delta \nu_{\text{calc}}^{\text{PAM}}$	$\delta \nu$	$\Delta \nu_{\text{calc}}^{\text{IAM}}$	$\delta \nu$	Transition $J_{K-K_+} - J'_{K'-K'_+}$	ν_{exp}	$\Delta \nu_{\text{exp}}$	$\nu_{\text{calc}}^{(\text{A}_1, \text{A}_1)} \Delta \nu_{\text{calc}}^{\text{PAM}}$	$\delta \nu$	$\Delta \nu_{\text{calc}}^{\text{IAM}}$	$\delta \nu$
(CH₃)₂⁸²Se													
$2_{11} - 2_{02}$	9864.538		9864.542	-0.004			$4_{23} - 4_{14}$	29494.137		29494.170	-0.033		
	9863.774	0.764	0.779	-0.015	0.781	-0.017		29491.634	2.503	2.388	0.115	2.387	0.116
	9863.030	1.508	1.562	-0.054	1.572	-0.064		29489.394	4.743	4.752	-0.009	4.746	-0.003
	9863.030	1.508	1.554	-0.046	1.553	-0.045		29489.394	4.743	4.799	-0.056	4.790	-0.047
$2_{21} - 2_{12}$	20147.367		20147.356	0.011			$5_{32} - 5_{23}$	20337.816		20337.812	0.004		
	20145.398	1.969	1.986	-0.017	1.972	-0.003		20335.924	1.892	1.897	-0.005	1.898	-0.006
	20143.776	3.591	3.604	-0.013	3.593	-0.002		20333.915	3.901	3.937	-0.036	3.926	-0.025
	20143.067	4.300	4.339	-0.039	4.295	0.005		20334.153	3.663	3.652	0.011	3.674	-0.011
$2_{12} - 1_{01}$	24788.250		24788.257	-0.007			$5_{23} - 5_{14}$	19720.730		19720.735	-0.005		
	24787.733	0.517	0.602	-0.085	0.604	-0.087		19719.350	1.380	1.371	0.009	1.377	0.003
	24786.965	1.285	1.193	0.092	1.199	0.086		19717.970	2.760	2.747	0.013	2.766	-0.006
	24786.965	1.285	1.216	0.069	1.219	0.066		19717.970	2.760	2.735	0.025	2.748	0.012
$2_{21} - 1_{10}$	38219.617		38219.594	0.023			$6_{33} - 6_{24}$	20510.406		20510.423	-0.017		
	38217.622	1.995	2.002	-0.007	1.990	0.005		20508.669	1.737	1.709	0.028	1.711	0.026
	38216.025	3.592	3.599	-0.007	3.589	0.003		20506.998	3.408	3.453	-0.045	3.469	-0.061
	38215.260	4.357	4.408	-0.051	4.370	-0.013		20506.998	3.408	3.383	0.025	3.387	0.021
$3_{21} - 3_{12}$	13324.051		13324.027	0.024			$6_{24} - 6_{15}$	27209.334		27209.271	0.063		
	13322.849	1.202	1.210	-0.008	1.205	-0.003		27207.608	1.726	1.748	-0.022	1.758	-0.032
	13321.601	2.450	2.483	-0.033	2.484	-0.034		27205.851	3.483	3.507	-0.024	3.516	-0.033
	13321.690	2.361	2.354	0.007	2.350	0.011		27205.851	3.483	3.483	0.000	3.506	-0.023
$3_{12} - 3_{03}$	15509.292		15509.313	-0.021			$6_{42} - 6_{33}$	31290.555		31290.543	0.012		
	15508.182	1.110	1.116	-0.006	1.121	-0.011		31287.829	2.726	2.638	0.088	2.734	-0.008
	15507.059	2.233	2.237	-0.004	2.242	-0.009		31284.262	6.293	6.317	-0.024	6.273	0.020
	15507.059	2.233	2.226	0.007	2.231	0.002		31285.904	4.651	4.238 ^C	0.413	4.660	-0.009
$3_{22} - 3_{13}$	24155.413		24155.402	0.011			$7_{43} - 7_{34}$	28009.339		28009.351	-0.012		
	24153.325	2.088	2.088	0.008	2.075	0.013		28006.703	2.636	2.613	0.023	2.637	-0.001
	24151.218	4.195	4.088	0.107	4.078	0.117		28003.864	5.475	5.513	-0.038	5.484	-0.009
	24151.218	4.195	4.233	-0.033	4.213	-0.018		28004.277	5.062	4.939	0.123	5.063	-0.001
$3_{13} - 2_{02}$	32965.037		32965.050	-0.013			$7_{34} - 7_{25}$	23776.280		23776.267	0.013		
	32964.515	0.522	0.528	-0.006	0.530	-0.008		23774.620	1.660	1.646	0.014	1.656	0.004
	32964.004	1.033	1.049	-0.016	1.061	-0.028		23772.950	3.330	3.300	0.030	3.336	-0.006
	32964.004	1.033	1.064	-0.031	1.071	-0.038		23772.950	3.330	3.281	0.049	3.301	0.029
$4_{22} - 4_{13}$	15095.993		15096.000	-0.007			$7_{43} - 6_{52}$	38556.865		38556.864	0.001		
	15094.782	1.211	1.216	-0.005	1.218	-0.007		B		-19.969		-16.437	
	15093.571	2.422	2.445	-0.023	2.463	-0.041		B		-6.567		-6.460	
	15093.571	2.422	2.420	0.002	2.419	0.003		B		-52.235		-43.937	
$4_{13} - 4_{04}$	23437.560		23437.560	0.000			$8_{44} - 8_{35}$	26473.624		26473.625	-0.001		
	23435.930	1.630	1.637	-0.007	1.642	-0.012		26471.341	2.283	2.266	0.017	2.281	0.002
	23434.270	3.290	3.283	0.007	3.283	0.007		26469.054	4.570	4.617	-0.047	4.633	-0.063
	23434.270	3.290	3.265	0.025	3.276	0.014		26469.054	4.570	4.449	0.121	4.496	0.074
$4_{32} - 4_{23}$	29757.233		29757.269	-0.033			$8_{35} - 8_{26}$	30407.815		30407.851	-0.036		
	29754.293	2.940	2.950	-0.010	2.904	0.036		30405.947	1.868	1.822	0.046	1.832	0.036
	29751.948	5.285	5.304	-0.019	5.285	0.000		30404.138	3.677	3.656	0.021	3.680	-0.003
	29750.898	6.335	6.497	-0.162	6.332	0.003		30404.138	3.677	3.631	0.046	3.664	0.013
$4_{31} - 4_{22}$	22273.190		22273.174	0.016			$9_{45} - 9_{36}$	28075.759		28075.744			
	22271.230	1.960	1.955	0.005	1.975	-0.015		28073.742	2.017	1.975	0.042	2.000	0.017
	22268.740	4.450	4.507	-0.057	4.473	-0.023		28071.744	4.015	3.971	0.044	4.031	-0.016
	22269.750	3.440	3.317	0.123	3.426	0.014		28071.744	4.015	3.928	0.087	3.984	0.031

A not resolved, B not measured, C not used for fitting.

Table 2. Rotational constants [GHz] and centrifugal distortion constants [GHz] for dimethyl selenide in the order of Table 1, calculated with equal sets of transitions of Table 1. The τ -centrifugal distortion constants [GHz] were derived from those of (1). Moments of inertia I_g [AMUÅ²] calculated with conversion factor $5.05376 \cdot 10^5$ AMUÅ² MHz [14]. α asymmetry parameter, in brackets doubled standard error, standard deviation [KHz] ninth line.

	⁷⁶ Se	⁷⁷ Se	⁷⁸ Se	⁸⁰ Se	⁸² Se
A	11.442978(7)	11.405953(8)	11.369972(16)	11.300409(19)	11.234103(12)
B	6.912763(7)	6.912807(8)	6.912844(17)	6.912862(19)	6.912885(13)
C	4.551511(6)	4.545652(7)	4.539929(14)	4.528768(17)	4.518053(11)
$\Delta_J \cdot 10^5$	0.492 (20)	0.611 (23)	0.932 (45)	0.808 (52)	0.722 (34)
$\Delta_{JK} \cdot 10^4$	-0.333 (6)	-0.323 (7)	-0.325 (13)	-0.330 (15)	-0.327 (10)
$\Delta_K \cdot 10^4$	0.869 (10)	0.847 (12)	0.847 (23)	0.852 (27)	0.840 (17)
$\delta_J \cdot 10^5$	0.339 (6)	0.348 (6)	0.345 (13)	0.341 (14)	0.345 (9)
$\delta_K \cdot 10^6$	0.27 (48)	-0.63 (55)	-0.35 (107)	-0.01 (121)	-0.43 (78)
	15	18	35	41	27
$\tau'_{aaaa} \cdot 10^3$	-0.234	-0.234	-0.246	-0.241	-0.234
$\tau'_{bbbb} \cdot 10^4$	-0.468	-0.523	-0.649	-0.596	-0.565
$\tau'_{cccc} \cdot 10^5$	0.744	0.337	0.966	0.506	0.124
$\tau_1 \cdot 10^4$	0.743	0.557	0.181	0.353	0.440
$\tau_2 \cdot 10^3$	0.348	0.207	-0.0771	0.0540	0.121
I_a	44.1647	44.3081	44.4483	44.7219	44.9859
I_b	73.1077	73.1072	73.1068	73.1066	73.1064
I_c	111.0348	111.1779	111.3180	111.5924	111.8570
α	-0.31473	-0.30990	-0.30515	-0.29586	-0.28683

Table 3. Correlation matrix of the fitted constants of Table 2 for (CH₃)₂⁷⁶Se. Most unfavorable case.

1.00								
0.49	1.00							
0.68	0.80	1.00						
0.48	0.02	0.45	1.00					
-0.13	0.25	-0.18	-0.89	1.00				
0.32	-0.34	0.10	0.92	-0.91	1.00			
-0.10	0.37	-0.15	-0.79	0.93	-0.83	1.00		
0.08	-0.27	0.16	0.81	-0.97	0.83	-0.96	1.00	

The IAM-analysis was performed according to the treatment of Woods [11, 12]. By a version of his program modified by Meier [13] and Lutz we got the results given in Table 5. $W(1)$ and θ was fitted.

The moment of inertia $I_a = 3.244$ AMU Å² of the methyl group was taken from [1] for both methods as I_a is strongly correlated to V_3 . The correlation coefficient of the two fitted parameters is about 0.7 in both cases.

	⁷⁶ Se	⁷⁷ Se	⁷⁸ Se	⁸⁰ Se	⁸² Se
s	42.11	42.14	42.13	42.13	42.16
F	166.146	166.115	155.083	166.033	166.002
V_3	1500.9 (19)	1501.7 (15)	1501.1 (13)	1500.7 (13)	1501.5 (14)
Θ	39.63 (16)	39.67 (13)	39.73 (11)	36.69 (11)	39.58 (12)
H	24	24	24	26	23
δ	70	56	48	49	52
$\overline{\Delta v}_{exp}$	2.923	2.936	2.937	2.710	2.894

Table 4. Internal rotation parameters of the PAM analysis for dimethyl selenide in the order of Table 1. $I_a = 3.244$ AMU Å² assumed. N Number of transitions, δ standard deviation of the fit [nHz], Δv_{exp} mean of splittings [MHz], s reduced barrier, F rotational constant of methyl-group [GHz], V_3 hindering potential [cal/mole], θ angle between internal rotation and a -axis [degree].

	⁷⁶ Se	⁷⁷ Se	⁷⁸ Se	⁸⁰ Se	⁸² Se
<i>W</i> (1)	-1.6112(77)	-1.6048(48)	-1.6060(47)	-1.6032(58)	-1.5988(51)
<i>s</i>	42.06 (3)	42.09 (1)	42.09 (2)	42.10 (2)	42.12 (2)
<i>F</i>	165.997	165.970	165.946	165.898	165.863
<i>V</i> ₃	1498.0 (13)	1498.8 (8)	1498.4 (9)	1498.4 (10)	1498.8 (9)
<i>Θ</i>	39.87 (11)	39.90 (7)	39.90 (7)	39.91 (9)	39.80 (8)
<i>N</i>	24	24	24	26	23
<i>δ</i>	51	33	31	37	36
$\overline{\Delta\nu}_{exp}$	2.948	2.960	2.962	2.783	2.920
<i>S</i>	0.06314	0.06297	0.06281	0.06250	0.06226
<i>Δ</i> ₀	-90.289	-89.892	-89.945	-89.766	-89.478
<i>β</i>	0.4674	0.4690	0.4704	0.4730	0.4737

Table 5. Internal rotation parameters of the IAM analysis for dimethyl selenide in the order of Table 1. *W*(1) Fourier coefficient see [5, 6, 11] *ϕ*, *Δ*₀[MHz], *β* [rad] IAM-Parameters [11] see also Table 4.

As can be seen from Tables 4 and 5 the values for the hindering potential *V*₃ and the angle *θ* between internal rotation and *a*-axis agree within the error limits for each method. As assumed no isotopic effect of the selenium substitution can be observed.

There is a slight difference between the results of both methods. The fit of the IAM seems to be superior to that of PAM indicated by the standard deviation. For single components we observed a good fit for IAM but not for PAM.

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